



UBERTONE

ultrasonic measurements in liquids

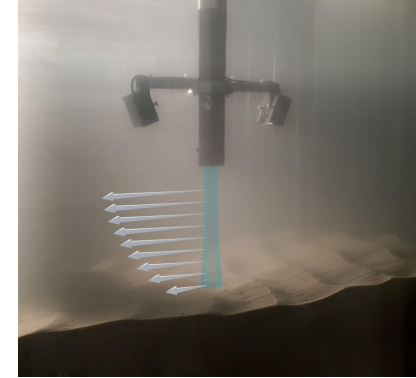


Turbulence Measurements with a New Two Components Ultrasonic Profiler

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Situation

- Need suspended solids measurement for environmental monitoring and industries
- LEGI: sediment transport monitoring in the lab
- UBERTONE: ultrasonic measurement in liquids



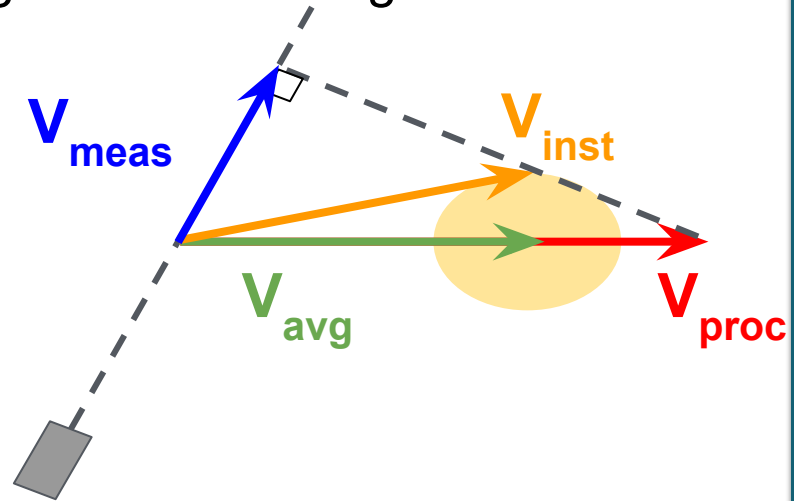
Goal

- Hydroacoustic inversion tool
→ concentration and grain size information
- Acoustic device



Ultrasonic Velocity Profiler

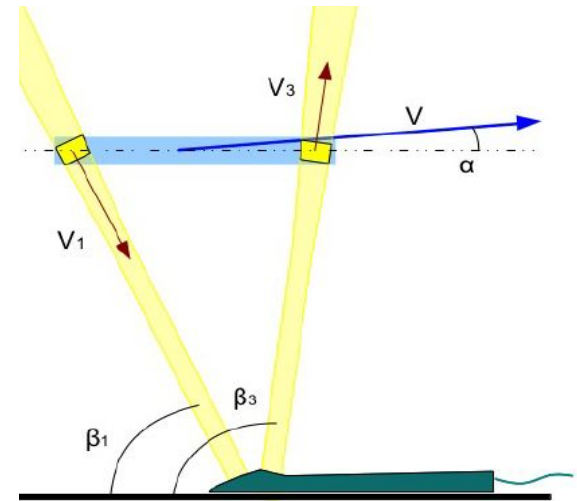
- UVP or UDV
- Pulsed Doppler : velocity profile along the beam at high resolution
- Accuracy : better than 0.34%
- needs **particles** / microbubbles
- clear and **opaque** liquids
- projected velocity on the beam axis
→ **1C mean** velocity profiling
uncertainty on flow direction
⇒ strong error on processed velocity



Furuichi, N. (2013). Fundamental uncertainty analysis of flowrate measurement using the ultrasonic Doppler velocity profile method. *Flow Measurement and Instrumentation*, 33, 202-211.

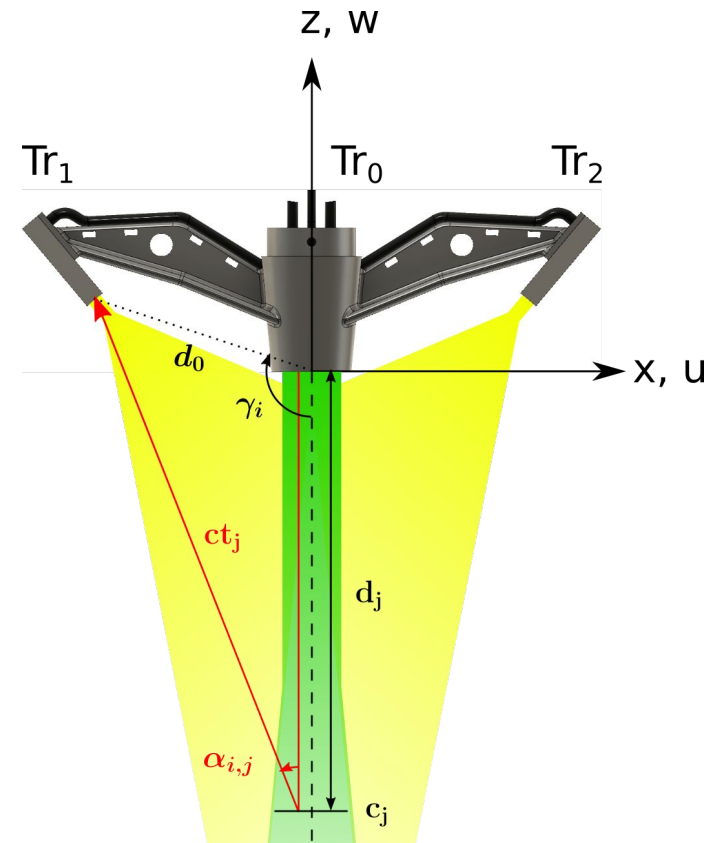
What about turbulent flow?

- UVP with multiple divergent beams
= multi-monostatic configuration
→ **2-3C/1D mean** velocity profiling
- UVP with beams grid
= multi-monostatic configuration
→ **2C/2D mean** velocity profiling
- **ADVP** (Acoustic Doppler Velocity Profiler)
= multi-bistatic configuration
→ **2-3C/1D quasi-instantaneous** velocity profiling



2C Bistatic Velocity Profile

- 3 transducers → 2 components **at the same time** in a profile along the beam
- Wide angle transducer : full profile of 2C velocity
- No side lobes effect



Hurther, D. et al. (2011). A multi-frequency Acoustic Concentration and Velocity Profiler (ACVP) for boundary layer measurements of fine-scale flow and sediment transport processes. *Coastal Engineering*, 58, 594–605.

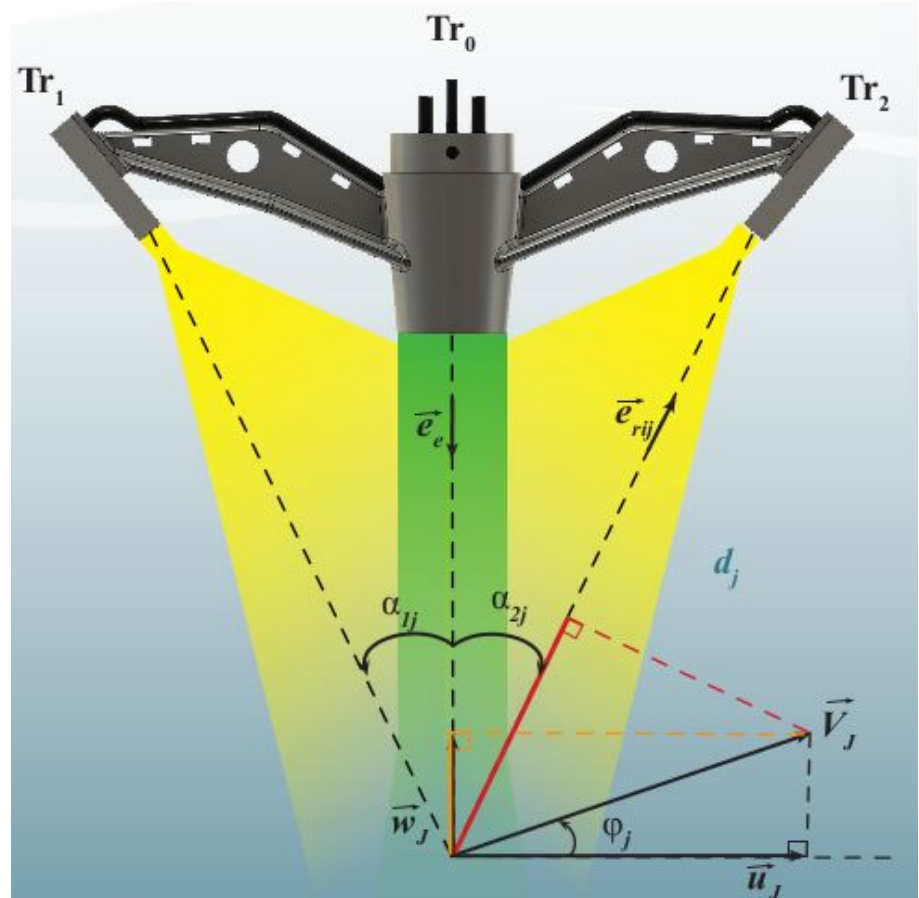
2C Bistatic Velocity Profile

$$V_{i,j} = \frac{cf_{d,i}}{f_0} = \vec{V}_j \cdot (\vec{e}_{rij} - \vec{e}_e)$$

$$= V_j (\sin(\varphi_j - \alpha_{ij}) + \sin \varphi_j)$$

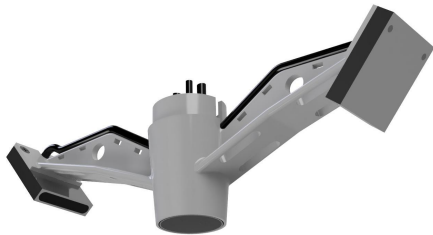
$$u_j = \frac{V_{1j} - V_{2j}}{2 \sin(\alpha_j)}$$

$$w_j = -\frac{V_{1j} + V_{2j}}{2(1 + \cos(\alpha_j))}$$



2018

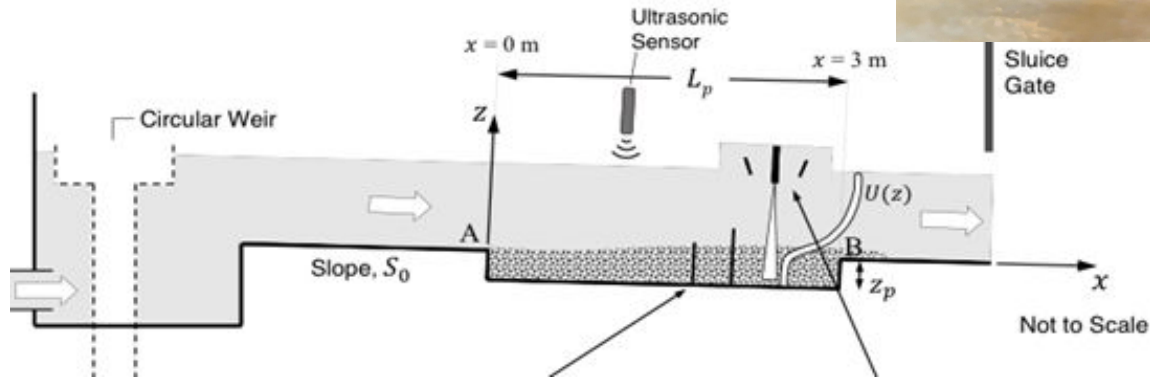
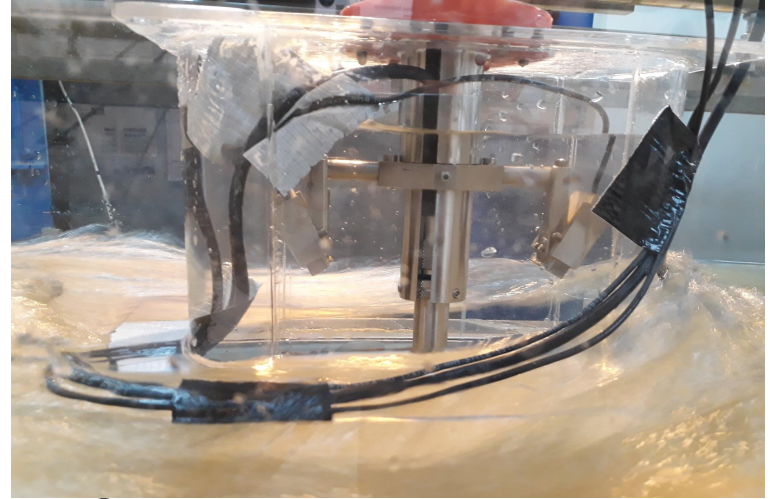
Acoustic Multi-Bistatic Profiler UB-Lab 2C



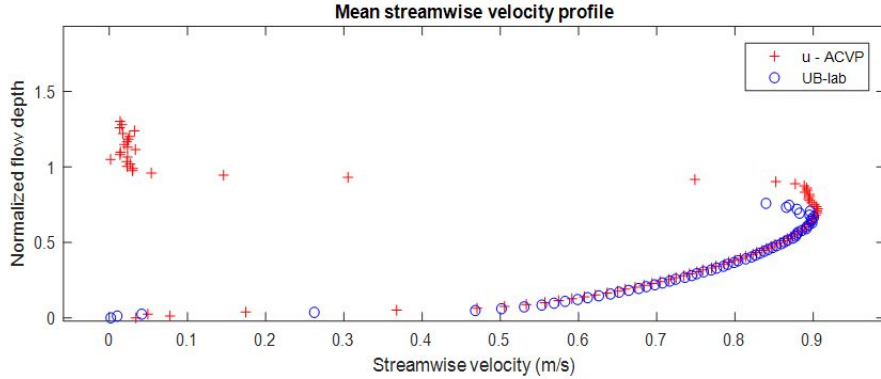
Emitting frequency	0.8 to 1.2 MHz
Spatial resolution	1.4 to 20 mm
Cells number	100
Transducers	1 Emitter + 2x2 Recievers
Temperature	1 input
Velocity accuracy	0.2 to 1 %
Sampling rate	100 Hz
Trigger	IN/OUT
Weight	1.5 kg
Consumption	4 W

2C measurement in a flume

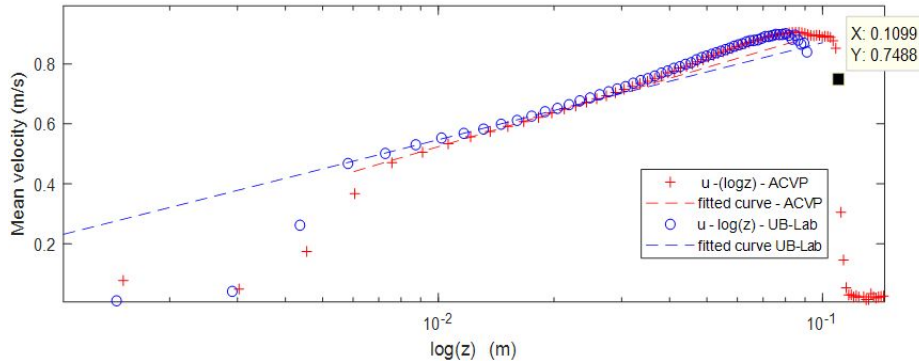
- UB-Lab 2C
- In a flume with sediment pit at the LEGI in Grenoble
- Reference measurement (not simultaneously) with ACVP



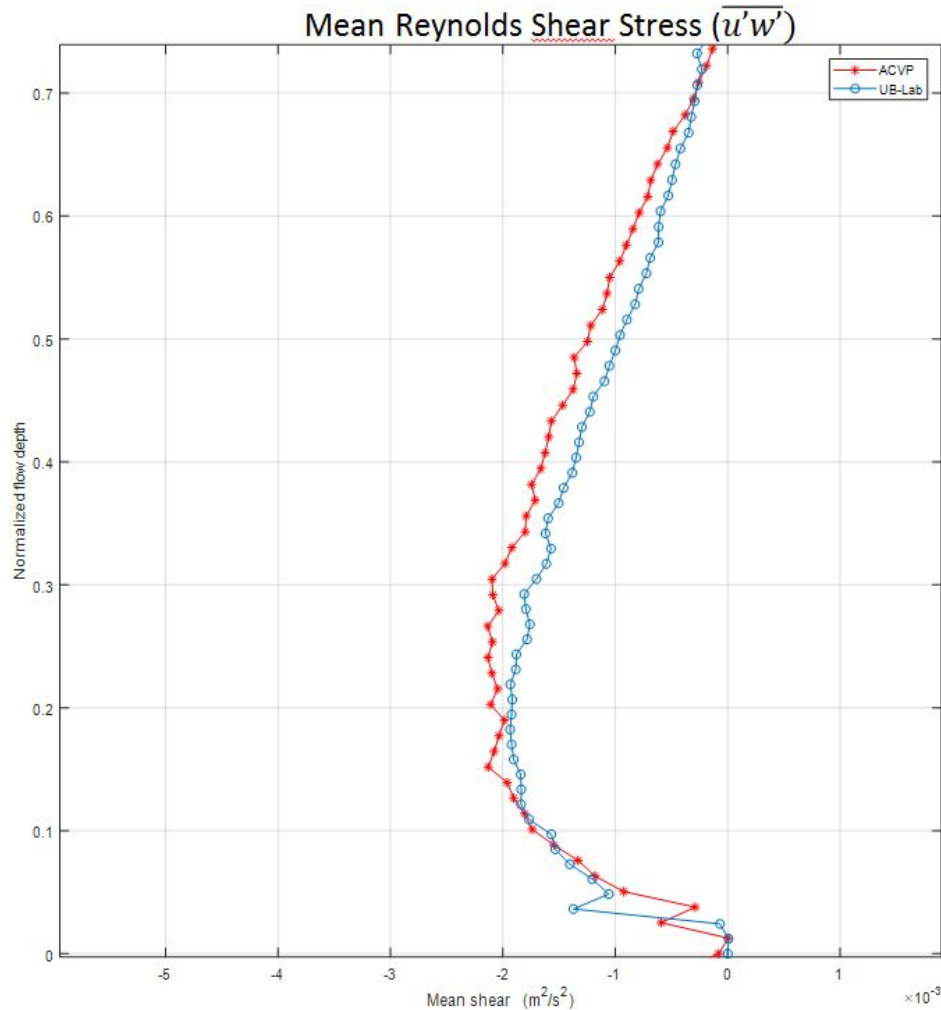
2C velocity profile



$$u = \frac{u^*}{k} \ln\left(\frac{z}{z_0}\right)$$



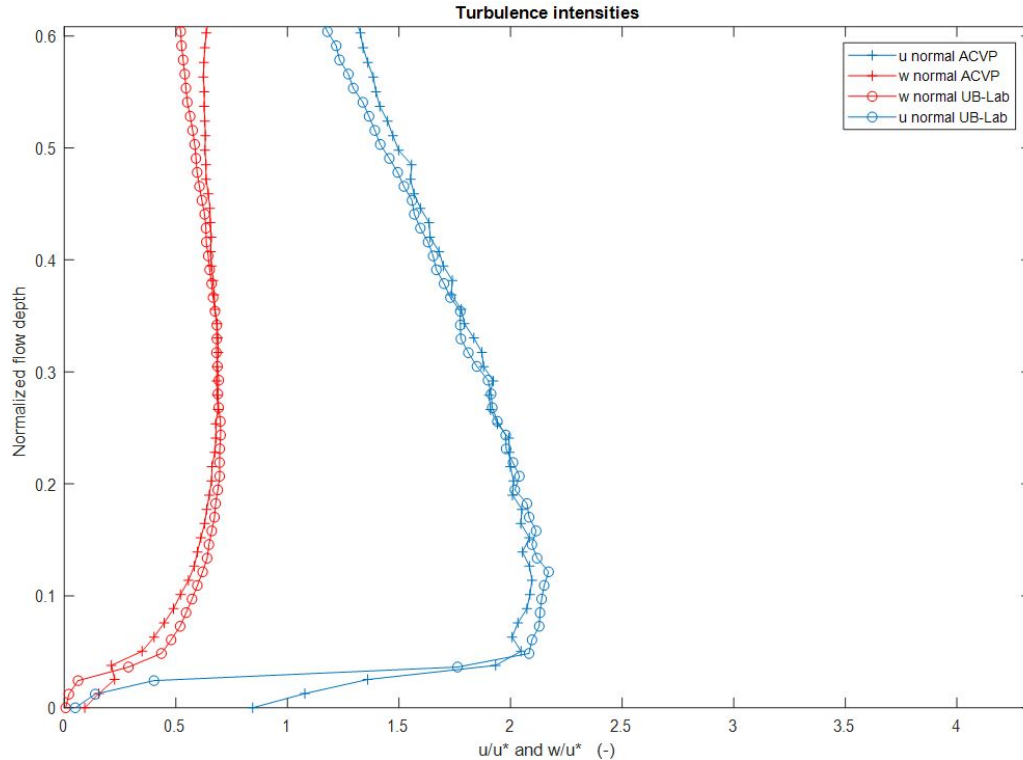
FRICTION VELOCITY	
	u*(m/s)
ACVP	0,060
UB-Lab 2C	0,057



Reynolds Shear Stress

- Higher friction velocity and higher shear stress for ACVP
→ higher flow rate
- 0 shear point not at $z/H_f = 1$
⇒ disturbance of the free surface flow due to sensor intrusion

Turbulence Intensities



$$u_{\text{rms}} = \sqrt{u'^2}$$

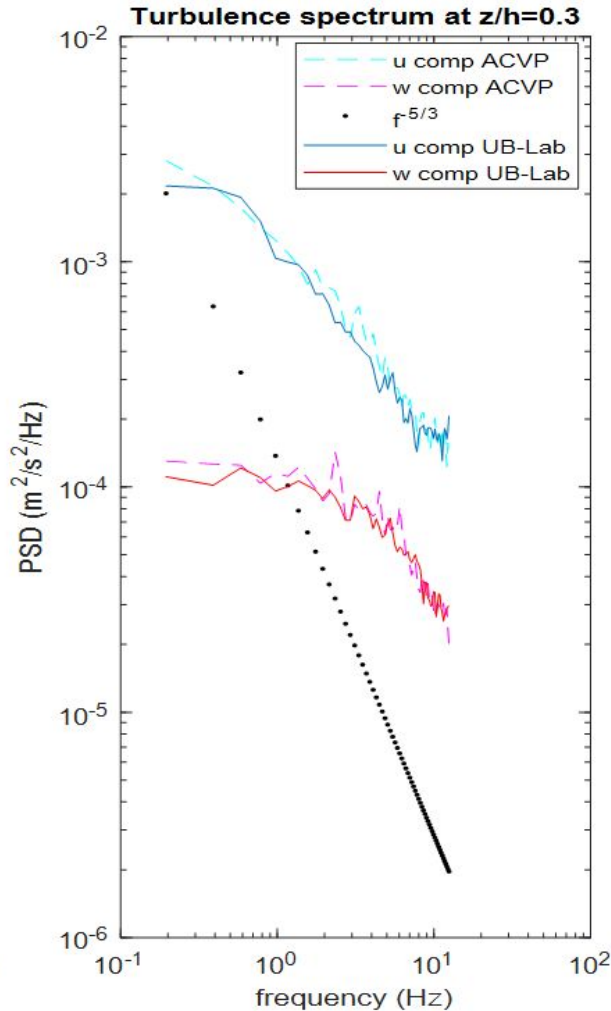
$$w_{\text{rms}} = \sqrt{w'^2}$$

- Good agreement of the system in both profiles u_{rms} and w_{rms}
- *Nezu & Nakagawa (1993)*

$$\frac{u_{\text{rms}}}{u_*} = 2.3 \exp(-C_u z)$$

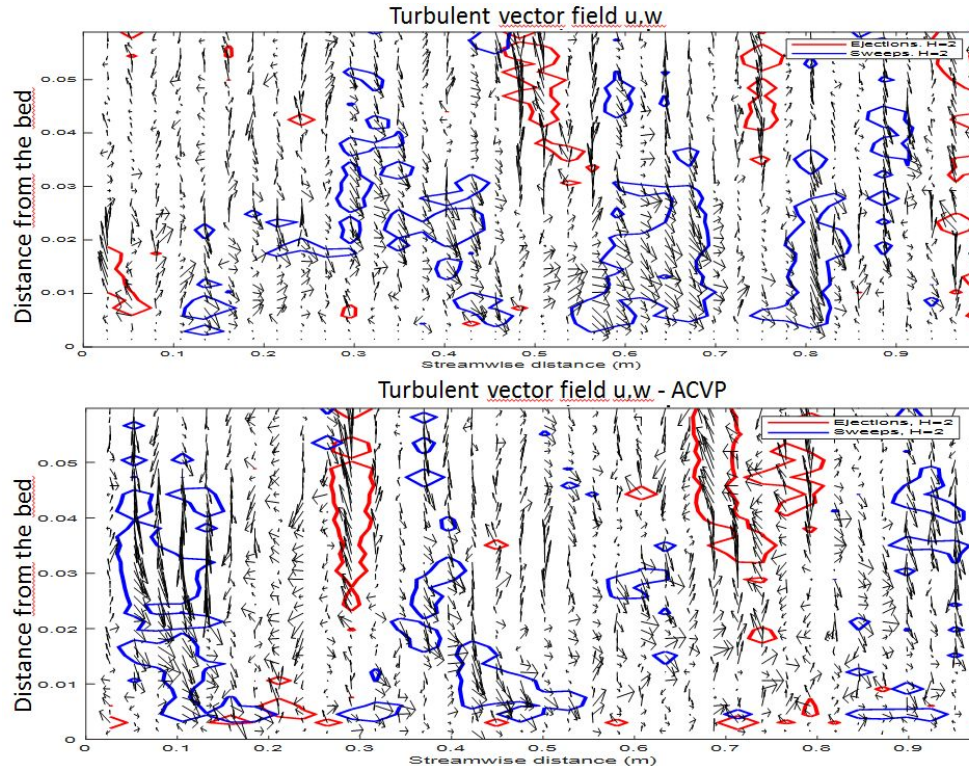
$$\frac{w_{\text{rms}}}{u_*} = 1.27 \exp(-C_w z)$$

Mean Turbulence Spectra



- Magnitude and shape of the Spectra are similar in both systems, for u and w
- Agreement with $-5/3$ slope confirms Kolmogorov (1941) turbulence cascading theory

Time resolved turbulence measurements



- Agreement between measurements of large scale turbulent flow structures: similar size, orientation and duration.
- True for both **Ejections** (red) and **Sweeps** (blue)

Conclusion

- Good agreement between the commercial UB-Lab 2C and the ACVP prototype of the LEGI
- And with previous measurement campaigns and literature
- **UB-Lab 2C** - instantaneous 2C-velocity profiles
- Next/ongoing:
 - comparing with LDA
 - measuring in pipe through a plastic wall

Thank you for your attention

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